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# VSR1 cavity finesse measurements 

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## 1 Introduction

The long cavities of the Virgo interferometer (north and west arms) consist in Fabry-Perot cavities when the interferometer is locked to take data in Science Mode. They are used to increase the power of the laser that is stored in the cavities.

The response of Virgo to a change in the cavity differential length is a modification of the laser power measured at the level of the dark fringe. It is defined as a transfer function in $\mathrm{W} / \mathrm{m}$.

When a cavity is locked, its response to a length modification behaves as a simple pole whose frequency depends on the finesse of the cavity. The average response of the cavities is taken into account in the reconstruction of the strain signal $h(t)$ to search for gravitationnal waves. The finesses of the cavities are expected to vary by a few percent as function of the mirror temperatures [1, 2].

The aim of this note is to estimate the variations of the finesses during the run VSR1 (May 18th to October 1st, 2007).

The method used to determine the cavity finesse, based on the comparison of the Airy peaks in the data with simulations, is described in the first section. The results and monitoring of the cavity finesse during VSR1 are then given. They are then compared to the variation of the power transmitted by the cavities.

## 2 Finesse reconstruction method

The finesse of the Fabry-Perot cavities depends on the mirror amplitude reflectivities $\rho_{1}$ and $\rho_{2}$ as:

$$
\begin{align*}
F & =\frac{\pi \sqrt{R}}{1-R}  \tag{1}\\
\text { with } R & =\rho_{1} \rho_{2} \tag{2}
\end{align*}
$$

The intensity reflection coefficients are defined as $r_{1}=\rho_{1}^{2}$ and $r_{2}=\rho_{2}^{2}$.
It can also be extracted from the $\mathrm{TEM}_{00}$ (Transverse Electro-Magnetic) Airy peaks [3]. Airy peaks are visible in the time variation of the power stored in the cavity when the length of the cavity changes. The powers in the north and west cavities are monitored through photodiodes in the external end-benches. The channel names are $\operatorname{Pr} \_\mathrm{B} 7 \_$DC and $\mathrm{Pr} \_\mathrm{B} 8 \_$DC respectively.

The finesse is defined as the ratio of the distance between two consecutive $\mathrm{TEM}_{00}$ resonances (FSR, Free Spectral Range) to their linewidth (FWHM, Full Width Half Maximum). However, due dynamical effects, the Airy peaks are distorted and the line width cannot be measured directly. The distorsion depends on the speed of the cavity mirrors. This parameter can be set in a dynamical simulation of a cavity which predicts the shape of the Airy peaks. A fit of the data with the simulation allows to estimate the finesse.

### 2.1 Estimation of the cavity length as function of time

The speed of the cavity is estimated from the cavity length time variation. The variation of the cavity length between two $\mathrm{TEM}_{00}$ resonances is equal to $\lambda / 2$ where $\lambda$ is the wavelength of the laser ( 1064 nm ).

An exemple of the cavity power as function of time is given in the figure 1. In order to reconstruct the cavity length time variations, the issue is to find the cavity length extrema. A few paremeters have been defined from three Airy peaks $(i-1)$ to $(i+1)$ around the current one indexed by $i$ : the amplitudes and widths of the peaks, $A_{j}$ and $W_{j}$, and the time between the peaks: $\Delta t_{j}=t_{j}-t_{j-1}$. The following conditions are used to define an extremum:

- when the Airy peak is at one extremum (speed close to 0 ), it is much larger than its neighbours: $W_{i}>2 W_{i-1}$ and $W_{i}>2 W_{i+1}$.
- when the Airy peak is after the lengh extremum and the extremum is close to next peak: $\Delta t_{i}>\Delta t_{i-1}$ and $\Delta t_{i}>\Delta t_{i+1}$ and $W_{i}>1.05 W_{i+1}$
- when the Airy peak is soon after the lengh extremum: $\Delta t_{i}<\Delta t_{i-1}$ and $\Delta t_{i}<\Delta t_{i+1}$ and $W_{i}>1.05 W_{i+1}$

If these conditions are not fulfilled, the cavity length is incremented by $\pm \lambda / 2$ depending on the current direction. An example of reconstructed cavity length time variation is shown in the figure 1.

If the cavity is excited but not too much (angularly and longitudinally), its length varies sinusoidally with time. A cosine function can be fit to the points: $l(t)=a_{i}+b_{i} \cos \left(\omega_{i} t+\Phi_{i}\right)$. For a given Airy peak at $t_{i}$, the fit is computed over a window of ?? s (or extended in order to enclose at least 5 peaks). The speed is then derived from $l(t)$ as $\left|v\left(t_{i}\right)\right|=b_{i} \omega_{i} \sin \omega_{i} t_{i}+\Phi_{i}$.

The cavity lenght can be reconstructed in different types of data.

- free swinging cavity: the cavity length variation is not really sinusoidal. The determination of its extrema, and therefore the cavity speed are not precise.
- swinging cavity with one mirror excited with a $\sim 1 \mathrm{~Hz}$ line. The cavity length variation is dominated by the 1 Hz excitation and the speed is reconstructed within $\sim 20 \%$.


Figure 1: Cavity power and estimated length vs time. (a) Reconstructed north cavity length variations for a dataset with specific injections. (b) Reconstructed cavity length variations in a short window, with the cosine fit. (c) Same, but with larger time window. (d) NE cavity power (Pr_B7_DC) as function of time in the same window as (b).

### 2.2 Simulation of the Airy peak shapes

The time domain simulation of a Fabry-Perot cavity including dynamical effects is computed using the SIESTA ${ }^{1}$ program [4].

A set of simulations are performed scanning the cavity speed and finesse from 0.5 to $30 \mu \mathrm{~m} / \mathrm{s}$ and 40 to 60 respectively, with steps of 1 for both parameters. The time serie of the simulated photodiode readout is sampled at $20 \tilde{\mathrm{k}} \mathrm{Hz}$.

Typical values of the mirror reflectivities (in intensity) are initially set to $r_{1}=0.882$ and $r_{2}=0.999957$. For a given cavity finesse, the reflection $r_{1}$ of the input mirror of the cavity is modified accordingly to equation 2 in the simulation. The speed of the cavity elongation is directly a parameter of the simulation configuration. An exemple of SIESTA configuration file is given in annexe.

For every sets of parameters (speed, finesse), the time serie of the simulated Airy peak is stored in a 3-dimension table within $\pm 0.020 \mathrm{~ms}$ ( 801 samples ) around the peak maximum. The amplitude of the peak is set such that the integral of the time serie is 1 . The shape of the Airy peaks is then lineraly interpolated between the different simulated sets in order to have a continuous function. The figure 2 shows the shape of the Airy peaks as function of the cavity finesse for a speed of $10 \mu \mathrm{~m} / \mathrm{s}$ and as function of the cavity speed for a finesse of 50 .


Figure 2: Shape of the simulated Airy peaks (a) as function of the cavity speed for a finesse of 50. (b) as function of the cavity finesse for a speed of $10 \mu \mathrm{~m} / \mathrm{s}$,

[^0]
### 2.3 Fit of the Airy peaks

Errors of $\pm 10^{-7} \mathrm{~W}$ have been used for the measurements of the cavity power time series Pr_B7, $8 \_$DC $\left( \pm 1.710^{-3}\right.$ V for the voltage time series $\left.\operatorname{Pr} \_B 7,8 \_d 1,2 \_D C\right)$. Every Airy peak $i$ detected in this time serie is fitted using MIGRAD ${ }^{2}$. The fit has four parameters: time of the maximum, amplitude, cavity finesse and cavity speed (when using the voltage channels Pr_B7, $8 \_d 1,2 \_$DC (in V), an offset is added as a fifth parameter).

The initial time of the peak is set to its maximum $t_{i}$. This parameter is constrained within $\pm 200 \mu \mathrm{~s}$ around $t_{i}$. The initial amplitude is set to the integral of the measured Airy peak. The initial value of the finesse is set to its nominal value of 50 . The initial speed of the cavity is set to the estimation described above. When the cavity length is close to a sine (with the 1 Hz excitation), the speed is constrained to vary by less than $30 \%$ from its initial value. Else, it is let free.

The Airy peaks with an estimated cavity speed outside the range $[3 ; 20] \mu \mathrm{m} / \mathrm{s}$ are not used.
A few cuts are applied in order to select the "good quality" fits.

- no error returned by MIGRAD,
- the parameters are not close to the edge of the simulated table,
- $\chi^{2}$ probability higher than $10 \%$.

[^1]
## 3 Measurements of the cavity finesse during VSR1

### 3.1 Measurements from Airy peaks in free swinging cavities

No specific data were taken during VSR1 to measure the finesse of the cavities. Datasets with free swinging mirrors have been selected. The criteria were at least 30 seconds (and maximum 500 seconds) of data in step 0 , with the BS and cavity mirrors aligned
(i.e. $S c_{-} N E$ _Gain_tyMarMis $=0$ ) and PR misaligned $\left(S c_{-} P R_{-} G a i n_{-} t y M a r M i s=\right.$ -150).

About 600 datasets have been selected during VSR1. The north and west cavity finesses have been fit using the voltage signal $\operatorname{Pr} \_\mathrm{B} 7 \_\mathrm{d} 1 \_\mathrm{ACp}$ and power signal $\mathrm{Pr} \_\mathrm{B} 8 \_\mathrm{DC}$ respectively. Since the cavities are not excited, the cavity motion is not well estimated. Thus the speed is let free in the Airy peak fits.

For every datasets, some checks are performed on a few distributions. Examples are shown in the figures $3,4,5$ and 6 . The mean of the distribution of the error-weigted fitted finesse is a way to measure the finesse of the dataset. The fitted finesse as function of the fitted speed (before the selection on the speed) is used to check that there is no correlation between both parameters. The relative difference between the fitted speed and its initial estimation is not really usefull since the initial estimation is rather bad. The difference between the fitted time of the maximum and its initial value is lower than $100 \mu \mathrm{~s}$.

The datasets are then selected using a few quality criteria. The number of correctly fitted Airy peaks must be higher than 100. Four estimations of the finesse are performed: the average values of the raw and error-weigted finesse distributions, the value from a Gaussian fit of the raw distribution and the median value of the fitted finesse. The differences between the values must be lower than 0.5 . The error of the Gaussian fit and the fitted sigma of the distribution must be lower than 0.5 and 1 respectively.

For the datasets passing the quality criteria, the finesses obtained from the Gaussian fit are given in appendix B and shown in the figure 7. Time variations are clearly visible, with amplitude of $\pm 1.5$ around the average value for both cavities. The average values obtain from the few measurements during VSR1 are 49.1 and 51.5 for the north and west cavities respectively.

### 3.2 Comparison with the locked cavity power variations

When the interferometer is locked (step 12), the north and west cavities are controlled such that the laser TEM00 mode resonates. The mirror relative positions are thus controlled such that the power that is stored inside the cavity is at a maximum of an Airy peak.

The power stored in the cavity, measured through the channels $\operatorname{Pr} \_\mathrm{B}\{7,8\} \_\mathrm{DC}$, is proportionnal to the cavity finesse. The relative variation of the cavity power gives a measurement of the relative variation of the cavity finesse.

The variations of the cavity powers in step 12 during VSR1 have been computed. They


Figure 3: Distributions for the north cavity at GPS 865551091. (a) Distribution of the error-weighted fitted finesse, finesse as function of speed, relative speed difference, time difference. (b) Distribution of the fitted finesse.


Figure 4: Distributions for the west cavity at GPS 865551091. (a) Distribution of the error-weighted fitted finesse, finesse as function of speed, relative speed difference, time difference. (b) Distribution of the fitted finesse.


Figure 5: Distributions for the north cavity at GPS 868086730. (a) Distribution of the fitted finesse, finesse as function of speed, relative speed difference, time difference. (b) Distribution of the error-weighted fitted finesse.


Figure 6: Distributions for the west cavity at GPS 868086730. (a) Distribution of the fitted finesse, finesse as function of speed, relative speed difference, time difference. (b) Distribution of the error-weighted fitted finesse.
have been normalised such that they match, on average, the finesse where there are direct measurements within one hour (normalisation factors of 575 and 627 for the north and west cavity powers respectively). The comparison of the finesse variations estimated by both methods are shown in the figure 8 . A zoom on the beginning of the run (figure 9), when the etalon effect changed by one period on the NI mirror due to temperature variations.

The behavior of the cavity finesse measured in this note and the transmitted power of the cavities are similar. It somehow validate the measurements using the Airy peak shape. However, two types of systematic errors can be highlighted:

- during periods with constant transmitted power value, the dispersion of the cavity finesse measurements is of the order of 0.2 ,
- the normalisation factor of the cavity power might change as function of time. It is expected to change due to different mirror and/or photodiode alignements. Using a constant normalisation factor during VSR1, differences up to 1 are seen between the normalized power and the finesse.


Figure 7: Finesse vs time during VSR1 for the west (black) and north (red) cavities. The lines gives the average values during the run.


Figure 8: Cavity finesse and normalised power transmitted by the north and west cavities. The transmitted powers have been normalised by 575 and 627 respectively.


Figure 9: Zoom on the cavity finesse and normalised power transmitted by the north and west cavities. During this period, the etalon effect of the NI mirror went along a full period due to high temperature variations.

## 4 Conclusion

The finesse of the north and west cavities have been measured during VSR1 using the shape of the Airy peaks seen in the transmitted power of the free swinging cavities. It permits to monitor the absolute value of the finesse and to estimate the amplitude of the finesse variation to about $\pm 2$ around their average values, as expected from the etalon effect in the input mirrors. Systematic errors of the order of 0.2 can be estimated from the dispersion of the measurements within short time-scales.

The variations of the measured finesse follow the variations of the power transmitted by the locked cavities. Differences of the order of $2 \%(\Delta F \sim 1)$ can be used as pessimistic systematic errors on the absolute value of the finesse using the Airy peak shape.

## References

[1] M. Punturo, The mirror resonant modes method for measuring the optical absorption (2007) VIR-001A-07
[2] M. Punturo, Etalon effect in the Virgo cavities, slides of weekly meeting from June 12th 2007
[3] F. Acernese et al. (Virgo collaboration) Applied Optics 46, Issue 17, pp 3466-3484 (2007). Measurements of the optical parameters of the VIRGO interferometer.
[4] B. Caron et al. Astroparticle Physics 10, 369-386 (1999). SIESTA, a time domain, general purpose simulation program for the VIRGO experiment.

## A SIESTA configuration file

Configuration file for the SIESTA simulation. In this simulation, the NE mirror is moving at $10 \mu \mathrm{~m} / \mathrm{S}$ (MISweep). The NE and NI reflection coefficients are respectively 0.999957 and 0.881968 The simulated finesse is thus 50 .

```
/* Creation of the clocks for signal simulation (rates) */
/* UJclock name totalTime nClocks Freq0 Freq1 */
UJclock masterClocks 80000 2 80000 1
```

/* Creation of the frame builder to store the output signals into a frame file */
UFrBuilder FBuilder 1100
/* ***** Creation of the mirrors with their surface ****** */

```
/* *** NI,back ****/
/*MIrror name clock susPos thermPos frontSurf backSurf initPos initOrientation */
MIrror Mir11 0 NULL NULL NULL MiSu11b 6.4 0.0. 1. 0. 0.
/* MIsurf name curvature radius thetaX thetaY halfThickness reflection losses */
MIsurf MiSu11b 0. .2 0. 0. 0. 0.881968 .1e-3
```

/* *** NE, front ****/
MIrror Mir12 0 NULL NULL MiSu12f NULL 3006.4 0. 0. 10. 0.
MIsurf MiSu12f $2.81294 \mathrm{e}-4 \mathrm{D}$ 0. 0. 0. 0.9999570.
/* *** WI, back ****/
MIrror Mir21 0 NULL NULL NULL MiSu21b 0. 5.6 0. 0. 1. 0.
/*MIsurf MiSu21b 0. . 2 0. 0. 0. 0 .1e-3 */
MIsurf MiSu21b 0. . 2 0. 0. 0. 0 0
/* *** WE, front ****/
MIrror Mir22 0 NULL NULL MiSu22f NULL 0. 3005.6 0. 0. 1. 0.
MIsurf MiSu22f $2.89855 \mathrm{e}-4$. 2 . 0. 0. 0 .
/* *** BS, front ****/
MIrror Mirbs 0 NULL NULL MiSubsf NULL 0.0.0. 1. -1. 0.
MIsurf MiSubsf 0. . 2 0. 0. 0. . 50 .
/* *** PR, front ****/
MIrror Mirrc 0 NULL NULL NULL MiSurcf -6. 0. 0. 1. 0. 0.
MIsurf MiSurcf 0. . 2 0. 0. 0. 0. 0 .

```
/* Define a mirror movement */
/* MISweep name clock mirror startPos slope(m/s) axis (0=x, 2=z) */
MIsweep sweepz 0 Mir12 0. 1e-05 2
/* Create the laser */
/*IOlaser name clock surf wavelength power noise noise curvature waist window method */
IOlaser laser 0 NULL 1.064e-6 . 56 NULL NULL 0. .021 .40 NO 0
/* Create the phase modulator */
OPmod mod 0 laser.oBeam 3 0. 6.26408e6 -6.26408e6 carrier NULL sb1 NULL sb2 NULL
/* Create the signals for amplitude modulation of the side bands */
USignal carrier 0.99
USignal sb1 0.075
USignal sb2 -0.075
/*dynamic simulation*/
OPglobal itf O mod.oBeam MiSubsf MiSu11b MiSu12f MiSu21b MiSu22f MiSurcf NO NULL
```

```
/* Create the photodiodes */
```

/* Create the photodiodes */
/*OPdiode name clock efficiency demodFreq demod incidentBeam withShotNoise? */
/*OPdiode name clock efficiency demodFreq demod incidentBeam withShotNoise? */
OPdiode B1 0 1. 6.26408e6 NULL itf.oBeam1 YES
OPdiode B1 0 1. 6.26408e6 NULL itf.oBeam1 YES
OPdiode B7 0 1. 6.26408e6 NULL itf.oBeam7 YES
OPdiode B7 0 1. 6.26408e6 NULL itf.oBeam7 YES
OPdiode B5 0 1. 6.26408e6 NULL itf.oBeam5 YES

```
OPdiode B5 0 1. 6.26408e6 NULL itf.oBeam5 YES
```

```
/* Simulate local readout */
/*UFrLRdout clock adcname input gain ADCbits type */
UFrLRdout 0 Pr_B7_DC B7.dc 1. -32 adc
UFrLRdout 0 Pr_B1_DC B1.dc 1. -32 adc
```

```
/* Save output to the frame file */
/* UFrOFile clock filename Ascii? frame framePerFile */
UFrOFile -1 finesse_tmp NO FBuilder.frameH 1
```


## B Measurements during VSR1

The measured finesse for all the selected datasets during VSR1 are given in the following tables for the west and the north cavities.
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| 04İ8t | 0890．0 干 067＊ 87 | 927 | －8¢9899998 | 008 ${ }^{\text {LG }}$ | OSLO 0 干 020 $0^{\circ} \mathrm{C}$ | 970I | － 782697798 |
| 082067 | 0才90．0 干 09\％ 67 | LZI | － 769798998 | 076＊${ }^{\text {LG }}$ | 0¢L0＇0 干 090． $\mathrm{CS}^{\text {c }}$ | LZLI | ＇tL2697t98 |
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| 08¢ LG |  | 961 | －67L90cti98 | 0¢t．LG | 09L0．0 干 00才゙ TG | 799L | － $009097 t 98$ |
| 009．LS | 0970 0 干 0L8． TG | ¢78 | －87970¢t98 | 07C．LG | 0070 0 干 077．LS | L97 | －L2898tt98 |
| 078． L $^{\text {c }}$ | 0LZ0＇0 干 $069^{\circ} \mathrm{T}$ ¢ | 298 | －67986も798 | 08L｀tc | 0070 0 干 0LE LS | 887 | －C067Ett98 |
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| 018．za | 08L0＇0 干 007． $\mathrm{C}^{\text {c }}$ | 992 | －0¢\＆66も798 | 060ㄴ．${ }^{\text {c }}$ | 0z80 0 干 0ZI＇LS | L6I | ＇も08\＆\＆tt98 |
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| 079 \％ | 0¢L0＇0 干 08L＇$\%$ ¢ | 622 | －008767798 | 0L0 TG | 08L0．0 干 028．09 | LLV | －288を8tø98 |
| 078． 69 | 0才L0＇0 干 $0600^{\circ} \mathrm{G}$ | 878 | －067667t98 | 0L2＇09 | 0LE0．0 干 099．09 | ¢¢\％ | －98078tt98 |
| 089＊L9 | OSL0＇0 干 020 79 | もも6 | －092067t98 | 02809 | 0080 0 干 082．09 | 907 | －999Lでも98 |
| 0L9＊LS | 0080＇0 干 $079^{\circ} \mathrm{TG}$ | 98\％ | －06968も798 | 0LZ＇LG | 0870 0 干 087 TG | 801 | －90czLtt98 |
| 0ga Ls | 09L0 0 干 07F＇LS | 068L | －08L687t98 | 02609 | 0GZ0＇0 干 06I＇TG | 9tI | －\％8\＆2Ltt98 |
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| 0LZ＊LS | 0070．0 干 $070 \cdot \mathrm{LG}$ | 607 | －GtLt8tt9 | 0L809 | 0880 0 干 $078^{\circ} 09$ | 02I | －980868t98 |
|  | 08L0＇0 干 07\％ $\mathrm{c}^{\circ} \mathrm{C}$ | 692 | －¢78LLtt98 | 0Lİ6t | $0090{ }^{\circ} 0$ 干 0G9 67 | LZI． | －¢L8928t98 |
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| 90．LS | 0LZ0＇0 干 080＇LG | 299 | － 890680898 | 078＊67 | $0070^{\circ} 0$ 干 $06 \varepsilon^{*} 67$ | L0I | －8LLIt0298 |
| 009．LG | 0¢\％0＇0 F 0¢L＇TG | L．9 | －0才7280898 | 008： 61 | 0L70 0 干 068.67 | 00I | － 766070298 |
| 026．09 | OGL0＇0 干 0 ¢0＇LS | 88もL | －08L980898 | 069＊6t | $0670^{\circ} 0$ 干 $027^{\circ} 6 \square^{\circ}$ | 798 | －¢99680298 |
| 008．LG | 08¢0 0 干 $07 \overbrace{}^{\circ} \mathrm{TG}$ | 897 | －090880898 | 006．67 | 08L0 0 干 $02 \varepsilon^{\circ} 67$ | 609 | －LL2880298 |
| 07¢ ${ }^{\text {L }}$ L | 06L0＇0 F 0¢E LG | 970 | － 766920898 | 0 LZ 67 | 08L0 0 干 $09767^{\circ}$ | ¢92 | － 269280298 |
| 096．09 | 0LE0＇0 干 08 L＇TG $^{\text {c }}$ | LLG | － 969920898 | 0LL＊61 | 08900 0 干 02 ® $^{\circ} 67$ | 08 I | －$\ddagger$ 66670298 |
| 079［9 | $0 ¢ \% 0^{\circ} 0$ 干 $007^{\prime}$ TS | 0.9 | － 688520898 | 009 67 | 06L0＇0 干 001 67 | 966 | －792870298 |
| 06İLG | 0才70＇0 干 08L＇tG | 689 | －0L0820898 | 099．8t | 08L0＇0 干 028．87 | 乙¢\＆L | －797870298 |
| 09L．LS | 0070 0 干 $069^{\circ} \mathrm{T}$ ¢ | もも8 | －8L9L69298 | 079．6t |  | 878 | L L0070298 |
| 060 7 C | 0\＆L0＇0 干 $079^{\circ} \mathrm{TG}$ | 078 | －867069298 | 0LL＊ 61 | 0090＇0 干 0076 6 ¢ | 875． | －068\＆28998 |
| 08t．09 | 0980 0 干 $06 \mathrm{~L}^{\circ} 0 \mathrm{C}$ | 991 | －809029298 | 00L＊6t | 07T0 0 干 0LI 6 万 | ILI | － 9 \＃も828998 |
| 08867 | 02L0＇0 干 09667 | 9 CL | －000299298 | 092＊8t | 0270＇0 干 089 ${ }^{\circ} \mathrm{C}$ | でも | －LE\＆L99998 |
| 02t0 0 c | 0LE0＇0 干 088.67 | 988 | －870099298 | 029＊8t | 0970 0 干 07I 67 | L゙6 | LLLZ89998 |
| 098＊67 | $0020{ }^{\circ}$ 干 $069^{\circ} 67$ | ¢9 | －¢¢6879298 | 02も゙ $6 \pm$ | $0770^{\circ} 0$ 干 $067^{\circ} 6 \square^{\circ}$ | 879 | －¢¢8もて9998 |
| 0L6．67 | 09โ ${ }^{\circ} 0$ 干 0L8 ${ }^{\circ} 6$ ¢ | ZIL | －ctiligla | 008：6t | $0270^{\circ} 0$ 干 $06 \nabla^{\circ} 6 \square^{\circ}$ | ¢09 | －¢99769998 |
| 0LL 67 | 0990＊0 干 007． 67 | 661 | －¢87809298 | 080 67 | $0870{ }^{\circ} 0$ 干 097＇67 | 969 | － 781 Lz9998 |
| 080．09 | 0870．0 干 0L6．67 | L81 | －tL096tz98 | 092．67 | 08L0 0 干 07 ® $^{\circ} 6$ 万 | 029 | －776079998 |
| 0L9．67 | OGSO＊O 干 OGL 67 | L8I | －69L887298 | 026．87 |  | GGg | －てLぃ079998 |
| 08867 | 0870 0 干 0 L6．67 | 9LI | －669896298 | 089＊6t | 09 ¢0＇0 干 00才 6 ¢ | 889 | －98も6［9998 |
| 096．87 | 0\＆L0．0 干 099．87 | 88LL | ＇ 76 L9LLL98 | 0¢8＊67 | $0770^{\circ} 0$ 干 $0 ¢ 77^{6} \square^{\circ}$ | 669 | －7828［9998 |
| 009．87 | $0720{ }^{\circ} 0$ 干 092．87 | 90I | － 88 ¢820298 | 079 67 | $0770{ }^{\circ} 0$ 干 $07 \overbrace{}^{\circ} 6 \square^{\circ}$ | 989 | －7278［9998 |
| 002：87 | 0才1．0 干 088 ${ }^{\circ} \mathrm{8T}$ | DIL | －0も¢990298 | 088＊6 | 09¢0 0 干 0 Lも 6 万 | 2.26 | －L269L9998 |
| 096＊87 | 0070．0 干 089．87 | 988 | － 0707990298 | 02866 | $0 ¢ 700^{\circ}$ 干 $02 \varepsilon^{\circ} 67$ | 629 | L6¢tL9998 |
| 089．87 | 0GL0＇0 干 $0699^{\circ} \mathrm{B}$ | 09I | －0¢2L90298 | 07I＊6t | $0 \varepsilon ¢ 00^{\circ}$ 干 $087^{\circ} 67$ | L6I | 6868 L9998 |
| 028＊87 | $0760{ }^{\circ} 0$ 干 $069^{\circ} 87$ | 00I | －L89L90298 | 070.67 | $0070^{\circ} 0$ 干 $087^{\circ} 67$ | L99 | 6LもEL9998 |
| 089．67 | $0 \searrow て 0^{\circ} 0$ 干 0¢\％ 6 万 | $\mp 99$ | －L6LE¢0298 | 078＊6 | 0LI0 0 干 07866 万 | 092 | －696zL9998 |
| 078．87 | 06L0＊0 干 090．67 | 6701 | －1897¢0298 | 069 67 | 0 LZ0＇0 干 $078^{\circ} 67$ | 679 | 69ちてL9998 |
| 099＊87 | 0LZ0．0 干 08L．87 | g7\％L | －LLLZ90298 | 02L＊6t | 0890．0 干 $07 \varepsilon^{\circ} 67$ | 701 | －98LZL9998 |
| ${\stackrel{\text { ип？}}{ }{ }^{\text {a }}}^{\text {H }}$ | ${ }^{72}{ }^{\text {f }}$ H | ${ }^{\text {ad }}$ N | Sdゆ | ${ }^{w}$ | ${ }^{72}{ }^{\text {f }} \mathrm{H}$ | ${ }^{p 2 d} N$ | Sdゆ |

Table 3：WE finesse measurements during VSR1（continued）．

| 087＊TG | 0LE0＊0 干 00¢．TG | 917 | －0L2879028 | 089．79 | 0680 0 干 $0 \angle 77^{\circ} 7 \mathrm{C}$ | LV9 | － 27 ¢¢68698 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 089．T9 | 08900 0 干 097．TG | 098 | － 977809028 | 078 69 | 0¢¢0 0 干 098.79 | 6L0L | －LEL768698 |
| 00\％ TG $^{\text {c }}$ | 0880＊0 干 0¢才．TG | 628 | －GLLL09028 | 0LL＇G9 | $0680{ }^{\circ} 0$ 干 $07 \varepsilon^{\circ} \mathrm{zc}$ | 267 | －LLLI68698 |
| 079．TG | 0¢70＇0 干 089 ${ }^{\text {TG }}$ | ¢L9 | －\％¢LT09028 | 00\＆ 79 | 0¢L0 0 干 067.79 | 66IL | － 229688698 |
| 072． 59 |  | L00］ | －769869028 | 070．7¢ | 0910 0 干 $078.7 ¢$ | 026 | －291688698 |
| 060．79 | 0LE0＇0 干 $0 \angle 88^{\circ}$ TS | 289 | －787969028 | 006．79 | 0980 0 干 0 Lち 7 ¢ | L8t | － 299888698 |
| 016．TG | 0¢70．0 干 0¢8．TG | 206 | － 797969028 | 0才L \％9 |  | 799 | － 2 İ888698 |
| 008．z¢ | 0070．0 干 08L＇TG | 26IL | －$冖 67659028$ | 098．79 | 0¢ $700^{\circ} 0$ 干 0 L® 7 C | 709 | －L29688698 |
| 006． L $^{\text {c }}$ | 0870 0 干 0LG＇TS | ZLIL | －786869028 | 0Lも 69 | 0610＇0 干 0LE $7 ¢$ | てぃ9 | －290788698 |
| 07L｀za | 0¢70＇0 干 0LI＇ZG | Ggi | －99866L028 | 02t79 | 0LE0＇0 干 07ヵ＇ 7 C | 677 | －299888698 |
| 00I• ¢¢ | 09L0＇0 干 080． $\mathrm{c}^{\text {c }}$ | ¢97 | － 766861028 | 080 $0^{\circ}$ |  | CLT | － 270888698 |
| 080 $0^{\circ} \mathrm{C}$ | 0もも0＇0 干 06I＇z¢ | モ0I | －LEE965028 | 009．$¢ 9$ | $0 ¢ 500^{\circ}$ 干 088.79 | T98 | －L¢9788698 |
| 070．z¢ | 0880 0 干 080 $0^{\circ} \mathrm{G}$ | 926 | －L69965028 | 00c．ts | 0880 0 干 $0999^{\text {L }}$ ¢ | 2IE | －T96888698 |
| 080 \％\％ | 0880 0 干 $0899^{\circ}$ TS | 675 | ＇もLE090028 | 009＊LS | 0850＇0 干 078．LG | 6LI | －6Lぃて\＆8698 |
| 072． $\mathrm{C}^{\text {c }}$ | 0890 0 干 07\％ 79 | 681 | －99L670028 | 0才6． T ¢ | 0LI0 0 干 00\％ 79 | LIL | －661678698 |
| 0¢0 $0^{\text {¢ }}$ | 0680＊0 干 078． $7 ¢$ | \％LE | －C99870028 | 008¢¢ | $02800^{\circ}$ 干 $029^{\circ} \mathrm{C}$ ¢ | 08I | －002082898 |
| 090．z¢ | 06900 0 干 088． 79 | GLI | －CtI870028 | 00L®¢ | 0たt0 0 干 $06 \mathrm{I}^{\circ} \mathrm{C}$ ¢ | 9Lt | －06L082898 |
| 0¢8＊${ }^{\text {LS }}$ | 0080\％ 0 干 078． $7 ¢$ | 687 | －989270028 | 096．79 | 00¢0＇0 干 00L 7 C | 90t | －089622898 |
| 086． L $^{\text {c }}$ | 0ZL0＇0 干 008． $7 ¢$ | 68LE | －G29t70028 | 00609 | 0870 0 干 $00 \varepsilon^{\circ} \mathrm{L}$ ¢ | $68 \%$ | －68け977898 |
| 0¢¢ \％${ }^{\text {c }}$ | 0920＊0 干 090＇z¢ | 701 | －こもで\％0028 | 0LG．ts | 0920＊0 干 091．L马 | LtI | －868もて7898 |
| 090\％\％ | 0060＇0 干 067． 79 | ¢0L | －818700028 | 027＊TS |  | 2，8 | －07676L898 |
| 002． ¢ $^{\text {c }}$ | 0790＊0 干 0LE $7 ¢$ | L\＆\％ | －862L00028 | 02L｀ts | $0 L 70{ }^{\circ} 0$ 干 $0 ¢ ¢^{\prime} \mathrm{LS}$ | 80t | －006L6L898 |
| 02L゙Z9 | 08G0＊0 干 067．7¢ | L\＆L | －882L00028 | 089＊09 | OLL0．0 干 0才6．09 | Lf8L | －068L6L898 |
| 087： 69 | 0980\％ 0 干 0LZ 79 | L¢\％ | －892666698 | 0L0 TG | 0LL0．0 干 07609 | 962I | －08806L898 |
| 070． 69 | 0¢T0 0 干 099 TS | 968 | －677888698 | 007＊TS | 0080 0 干 $079^{\circ} \mathrm{T}$ ¢ | L0t | －020cli898 |
| 092＊LS | 0960 0 干 087＇LS | 6， | －090LL9698 | 096．ts |  | モ0t | －099tLI898 |
| 018．79 | 0LL0＇0 干 088． 7 C | ¢¢ | －62IStt698 | 079＊LS | 0¢E0＇0 干 0g\％LG | 899 | －0才C8LL898 |
| 018． 5 | 0LZ0＇0 干 0¢T＇ 7 C | \＆L¢ | －L688tt698 | 00c．ts | 0970 0 干 0¢0＇LS | L69 | －876960898 |
| 067．${ }^{\text {c }}$ | 0¢ $200^{\circ} 0$ 干 087．7c | 781 | －79188t698 | 00609 | 0¢80 0 干 $0688^{\circ} 09$ | L®\％ | － 7 ¢8760898 |
|  | 0990＊0 干 0L6． LG $^{\text {c }}$ | 847 | ＇78780п698 | 097＇ L9 $^{\text {c }}$ | 0870 0 干 $0 ¢ \varepsilon^{\circ} \mathrm{L}$ ¢ | Ø¢ | －¢0L060898 |
| ${ }^{\text {иппрәи }}$ H | ${ }^{727}{ }^{\text {H }}$ |  | Sdゆ | ${ }^{\text {ип！рәш }}$ H | ${ }_{7}^{72}$ H | ${ }^{\text {sybad }}$ N | Sdワ |

Table 4：WE finesse measurements during VSR1（continued）．

|  | 0¢L0＊0 干 0¢9 \％¢ | 979 | －20才0¢0¢28 | 0¢L｀TG | 0¢Ћ0．0 干 $0 \pm 8^{\circ} \mathrm{LG}$ | 08L | 669z987 28 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0L9．z¢ |  | 27.6 | －L2t670928 | 068 ${ }^{\text {TG }}$ | 0¢E0＇0 干 $0266^{\text {L }}$ LG | 0LI | 920798t 28 |
| 099．z9 |  | 0 L\％ | 698870928 | 078＊${ }^{\text {LG }}$ | OGL0＇0 干 $078^{\text {c }}$ LG | 676 | 0LLT98t 28 |
| 028\％9 | $986000 \% 089^{\circ} 79$ | 982 | －688L70928 | 069 ${ }^{\text {TS }}$ | 0才て0＇0 干 062． TG | 927 | －¢¢0T98t 28 |
| 089．7¢ | 06L0．0 干 0Gc $\%$ c | 981 | －0才LL70928 | 082．TG | 0LZ0＇0 干 08L＇LG | 281 | 696678728 |
| 089．79 | 09L0．0 干 069． 79 | 29I | －DL0LZ0ç8 | 098．LG |  | 97. | － 908678728 |
| 008． 79 |  | 7\％\％ | － 009970928 | 0 St LG | 0680 0 干 $009^{\text {TG }}$ | ¢¢L | －262678728 |
| 097． $\mathrm{c}^{\text {c }}$ | 08L0．0 干 099．7c | 20I | －027970928 | 078 ${ }^{\text {LS }}$ |  | 789 | －¢19678728 |
| 079 79 |  | \＆69 | －09z9z0c28 | 008＊LG | 09E0＇0 干 0LE LG | 981 | －6L8878t28 |
| 029\％9 | OちZ0＇0 干 0LL． 79 | モ81 | －0才Lもて0928 | 089．6ஏ | 07L0 0 干 099．67 | 29IL | －96I688728 |
| 0LL $\mathrm{Ca}^{\text {c }}$ |  | ¢92 | －0¢Zって0928 | 070．09 | 08L0．0 $\mp 076.67$ | 987 | －969088728 |
| 068．79 | 79900 0 干 $09 \varepsilon^{\circ} \mathrm{ZG}$ | 0L8I | －072870928 | 0才t．09 | 0LL0 0 干 $0688^{6}$ | 9L0I | － 9 L0088728 |
|  | 00L0．0 干 0¢\％\％ 9 | $\pm 09$ | －¢¢も¢z0g28 | 096．67 | 00L0 0 干 $0 \mp 8^{\circ} 67$ | 087I | － 909678728 |
| 070． Ca | 0才L0．0 干 001． 7 c | 0L9 | －I¢97\％0928 | 000．09 | 09L0 0 干 0 88.67 | 689 | 966878728 |
| 096．T¢ | 09L0．0 F 078．LG | 988 | －LZLZ70928 | 069．79 |  | 991 | 006987ヶ28 |
| 0LE \％9 | 0080＊0 $\ddagger 067^{\circ} \mathrm{ZG}$ | 0 L\％ | －¢866L0928 | 090 ${ }^{\circ} \mathrm{c}$ | 0090＇0 干 097 $7 ¢$ | 926 | 0289¢7t 28 |
| 0LZ．79 | 0870＊0 干 07\％＇7¢ | get | －8088L0928 | 096．LG | 0LI0＇0 干 0L9 LG | 978 | 09282LtL8 |
| 07L｀¢¢ | 0970＊0 干 07\％＇z¢ | L0\％ | －9898L0928 | 091．09 | 0670 0 干 $0 \pm L^{\circ} 09$ | ¢St | －86L7078L8 |
| 068．79 |  | \＆L\％ | －8898L0928 | 0L9＊8t |  | 961 | －289LLIEL8 |
| 098．79 | 0¢70＊0 干 0¢\％＇z¢ | 978 | － 6622 L0928 | 006．67 | 0¢L0＇0 干 070．09 | 701 | － 7 ［ち98Lで28 |
| 0も6．T¢ | 0\＆L0＊0干0¢LTG | LZ0］ | －609910928 | 079．09 | 0090＊0 干 080．09 | 29I | － 706982 L 28 |
| 06L．t9 | 07\％0＇0 干 09L＇TS | 979 | －8998L0cz8 | OtE09 | 07ヶ0＇0 干 020．09 | $\underline{4} 9$ | －¢1898LzL8 |
| 0¢E TG | 0LZ0＊0 F 069 $^{\text {LG }}$ | モ¢¢ | －gccilogz8 | 001．09 | 0070 0 干 0L0．09 | ¢67 | －¢67ヵ¢LzL8 |
| 07¢． Cc | 09L0＊0 干 098． $7 ¢$ | て，9 | －880900928 | 087＊67 | $0 ¢ ¢ 0{ }^{\circ} 0$ 干 $0666^{\circ}$ | 807 | －Tも706çz |
| 08L｀ ¢9 $^{\text {c }}$ | 0才L0：0 干 08E． 79 | 296 | －¢69900cz8 | 0L0 LG | 0LZ0＇0 干 0¢\％＇LG | \％L2 | －69LL99028 |
| 080 ${ }^{\text {tg }}$ | 06L0．0 F 0tE L | 078 | －¢9才700¢ 28 | 098．LG |  | ఒ〒\％ | －$¢ 7889028$ |
| 062．tc | 08L0 0 干 $000 \cdot 69$ | 966 | － $999988 \pm 28$ | 089 ${ }^{\text {TG }}$ | 00¢0 0 干 $069^{\circ} \mathrm{LG}$ | $67 \%$ | －¢¢Lec90 ${ }^{\text {c }}$ |
| 089 ${ }^{\text {T }}$ ¢ | 0¢70＊0 干 0¢8．LG | ¢99 | －¢96988728 | 020．7s | OtL0 0 干 $029^{\circ} \mathrm{TS}$ | 768 | 702LE9028 |
| 07L $\mathrm{c}^{\text {c }}$ | 0770＊0 干 029 LS | ¢88 | － 990988728 | 0St．LS | 00¢0＇0 F 0¢G＇LG | L98 | －872679028 |
| 089 ¢¢ |  | $68 \%$ | －28t998t 28 | 0tL．ts | 07L0．0 干 067＊LS | 8791 | －887679028 |
|  | ${ }^{727}$ H | ${ }^{\text {sybad }} N$ | Sdワ | ${ }^{\text {uпpp }}{ }^{\text {a }}$ H | ${ }_{7}^{72}$ H | ${ }^{p a d} N$ | Sdゆ |


－иวп！b วıд


| 08L＊67 | 0¢E0＊0 干 0L6．87 | 089 | －80L889LL8 | 098＊87 | 0880＊0 干 098．87 | †¢9 | －9818L0L98 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 097：67 | 0970．0 干 026．8才 | 988 | －869289LL8 | 086．87 | 0290．0 $\mp 08 L^{\circ} 87$ | $67 \%$ | －¢02910298 |
| 0¢6＊8t | $0770 \cdot 0$ 干 006.87 | 6I0I | －880289LL8 | 029＊8t | 0もモ0．0 干 0¢L．8̇ | \＆Lt | －0098L0298 |
| 0TL＊8t | $0 ¢ ¢ 00$ 干 0\％L＇8t | てワ8 | －890989L28 | 007＊6】 | $00 ¢ 00^{\circ}$ 干 0\＆6．87 | LUt | －L0L9L9998 |
| 078＊8t | 0L60．0 $\mp 060 \cdot 8 \pm$ | 68I | －2LL909028 | 088＊ 8 t | 0¢E0．0 干 $078.8 \pm$ | L09 | －L69tL9998 |
| 080 2 t |  | ¢ヵI | － 78 Lt09028 | 007＊ $6 \pm$ | $0 ¢ ¢ 00^{\circ}$ 干 076．87 | 797 | －6967L9998 |
| 092： 2 t | 091．0 $\mp 08 L^{\circ} \mathrm{LE}$ | 87I | － 7 Lece9028 | 098．87 |  | 087 | －8LLLL9998 |
| 078： 27 | $09600^{\circ}$ 干 0L6 2 L | LLI | － 709709028 | 072：87 | $0070 \cdot 0$ 干 0LL．87 | 276 | －88c89¢998 |
| 060＊8t | 09L0．0 干 0ZI．8t | 897L | － $7 \pm 9669028$ | 0\＆¢ 67 | $00700^{\circ}$ 干 00才 6 ¢ | DLS | － 787698998 |
| 067＊ 27 | 09200 干 0才8． 2 L | ¢67 | －709269028 | 092009 | 0LI＇0 干 070＇LG | 86I | －L60LGç98 |
| 088． 2 t | $08700^{\circ} \mathrm{F} 098^{\circ} \angle \mathrm{L}$ | 967 | － 797 969028 | 067＊6ワ |  | 998 | － 79289 ¢798 |
| 098.87 | 0GS0．0 干 029．87 | $88 \%$ | －8LLL66698 | 009＊87 | 08900 干 029．87 | 899 | － 702997798 |
| 061＊6t | 0TE0．0 干 09L．8才 | 986 | －2L9988698 | 068＊8t | 0980 0 干 00¢ 6 万 | 916 | －¿\＆Lz9tt98 |
| 067＊67 |  | $99 \%$ | －8908L8698 | 086．87 | 0270．0 $\mp 076.87$ | 988 | － 76009 ¢798 |
| 067＊6ヵ | 08L0＇0 干 0LI 6 万 | 881 | －T968¢8698 | 00867 | $0 ¢ \mp 00^{\circ} 0$ 干 $096.8 \pm$ | 898 | －L2898t798 |
| 0 ［9．67 |  | 70I | －6Lちて¢¢698 | 001＊6t | 07900 干 096．87 | 0¢\％ | －67678tt98 |
| 069＊8t | 0LLO 0 干 0906 6 万 | CEL | －0¢もて 68698 | 062：87 | OGL0＇0 干 028．87 | ¢ZI | －98078tt98 |
| 076． 27 | 09才0．0 干 069 2 L | 298 | －89L260898 | 098．87 | $0990{ }^{\circ} \mathrm{F}$ 干 000 6 б | ¢\＆L | －999LZっt798 |
| 069． ¢ $^{\text {¢ }}$ | 0LG0 0 干 0LL 2 L | 027 | －¢02060898 | 076：87 | $08700^{\circ} \mathrm{F} 000{ }^{\circ} 6$ 万 | もLI | － 788 LIt 98 |
| 088＊87 | 0LI0 0 F 0L8 2 L | 928 | －0才てL80898 | 029＊8t | $0970{ }^{\circ} 0$ 干 006．87 | 006 | －88¢9LIt98 |
| 02L： 2 T |  | LLL | －0¢L980898 | 0L9 6 6 ¢ |  | $67 \%$ | － 96 L766898 |
| 096． 2 t | $00 才 0 \cdot 0$ 干 0\＆L 2 L | 809 | －209080898 | 07E6も | $08 L 0 \cdot 0$ 干 $0 \varnothing \sim \cdot 67$ | 907 | －60LL88898 |
| 097＊ 2 も | $00600^{\circ}$ 干 $0 屯 9 . \angle \square$ | モ¢\％ | －096990898 | 07\％＊09 | 0も才0．0 干 088．6ぁ | ๕¢\％ | －669088898 |
| 086．87 | 0990．0 $\mp 00067$ | L\＆\＆ | －L6LE90298 | 029 6t | 0L90．0 干 079 6 6 万 | 881 | －600928898 |
| 001＊6t | 07T0 0 干 0L0 67 | 819 | －L89790298 | 002＊6t | 0LZ $0^{\circ} 0$ 干 098 ${ }^{\circ} 67$ | 88\＆ | －66もGL8E98 |
| 096＊8t | 0870.0 干 080 67 | ¢68 | －8もちで0298 | 097＊67 | 0L90．0 干 0\＆66 6 万 | 69 I | －62tもL8898 |
| 09I＊6t | 0ZI．0 干 018．87 | ZIL | －6LLZた0298 | 02967 | $08100^{\circ}$ 干 $0766^{6}$ | 799 | －68ちて28898 |
| 009＊87 | 0LE0 0 干 0L0 67 | LE8 | －207880298 | 078 6 ¢ | 02I0 0 干 0\＆66 6 万 | ஏ98 | －676L28898 |
| 026＊8t | $0 ¢ ¢ 00$ 干 08L 87 | 7.29 | － 798870298 | 090＊09 |  | 998 | －606028898 |
| 091：6t | 0790.0 干 $066.8 \pm$ | \＆LI | －L0070298 | 0L6．61 | 00L0．0 干 0L8．6才 | 892 | $\cdot 668028898$ |
| ${ }^{\text {ипррәш }}$ H | ${ }^{7 ?}$ | ${ }^{\text {sypad }} \mathrm{N}$ | Sdゆ | ${ }_{\text {ипррәш }}$ H | ${ }^{72 f}{ }^{\text {H }}$ | ${ }^{\text {sypad }}$ N | Sdわ |



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|  | $\mathfrak{t}$ |
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[^0]:    ${ }^{1}$ SIESTA version v4r00

[^1]:    ${ }^{2}$ GRADiend MInimisation

